

APPLICATION FOR UNITED STATES LETTERS PATENT

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TITLE: OPTOELECTRONIC APPARATUS

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CROSS REFERENCE TO RELATED APPLICATION

[1] This application claims the priority of German Application No. 100 36 538.8 filed July 27, 2000, which is incorporated herein by reference.

BACKGROUND OF THE INVENTION

[2] The invention relates to an optoelectronic apparatus having a transmitter that emits transmission light, a receiver that receives reflected light, and an evaluation unit, in which the transit time t_0 of the transmission light that is guided in the monitored region and reflected back, as a reflected light, by an object is evaluated for determining the distance of the object.

[3] An optoelectronic apparatus of this type is known from DE 43 41 080 C1. For locating objects in a monitored region, the optoelectronic apparatus has a transmitter that emits transmission light beams, and a receiver, which is embodied as a location-resolving detector and receives reflection light beams, the transmitter and receiver being integrated into a common housing. The transmission light

beams are diverted by a diverting unit, and periodically guided inside a monitored region. A phase measurement is employed in determining the distance of objects in the monitored region. The phase measurement is used to determine the transit-time difference of the received reflection light beams reflected by an object relative to the transmission light beams emitted by the transmitter.

[4] Outside of the monitored region, a test object is disposed inside the housing. For checking the function of the optoelectronic apparatus, the transmission light beams that the test object reflects back to the receiver as reflection light beams are evaluated in terms of their amplitude in an evaluation unit.

[5] Thus, it is possible to verify whether the transmitter or receiver is functional. Disturbances caused by the aging or contamination of components can also be ascertained with the test measurement using the test object.

[6] The test measurement using the test object is not, however, conclusive in terms of whether the distance measurement for locating the objects in the monitored region is error-free. The test measurement cannot

eliminate errors that may occur in the distance measurement.

SUMMARY OF THE INVENTION

[7] It is an object of the invention to embody an optoelectronic apparatus of the type mentioned at the outset to assure the highest possible precision and most reliable verification in objects in the monitored region.

[8] The optoelectronic apparatus according to the invention accomplishes this object with the transmitter emitting the transmission light in the form of a sequence of transmission light pulses where a portion of the light quantity of a transmission light pulse is coupled out as a reference transmission light pulse and guided by way of a reference path to the receiver; and an evaluation unit determines the transit time t_R of the reference transmission light pulse guided as a reference reflected light pulse to the receiver and the transit-time difference $t_o - t_R$ to determine the distance of an object.

[9] That is, the optoelectronic apparatus of the invention has a distance sensor that operates according to the pulse-transit-time method. The distances of objects

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[13] The evaluation of the transit-time difference $t_0 - t_R$ extensively eliminates internal measurement errors occurring in the distance measurement. One cause of such measurement errors is that the emission of a transmission light pulse does not occur simultaneously with the actuation of the transmitter due to a trigger pulse or the like. Instead, the transmission light pulse is emitted with a slight delay due to the finite transit times of the electrical signals in the individual components. These transit times exhibit variations as a result of fluctuations in temperature or operating voltage, or because of aging of the components.

[14] The same is true for the registration of the reflected light pulses at the receiver. The conversion of the pulses into electrical reflection signals, and their amplification, is affected by delay times, which are likewise subjected to fluctuations caused by interfering influences.

[15] In the ascertainment of the transit times t_0 for determining the distance of objects in the monitored region, and the determination of the transit times t_R in the reference measurement, the same delay times that are affected by fluctuations are superposed over the distance-

measurement values. These disturbance-influenced delay times are eliminated in the formation of the transit-time difference $t_o - t_R$, which considerably increases the precision and reproducibility of the distance measurement.

[16] A particular advantage is that the referencing of the distance measurement is performed continuously for all of the transmission light pulses guided into the monitored region.

[17] This advantage is also attained if a diverting unit periodically guides the transmission light pulses into the monitored region. Then, for creating a reference measurement for each diversion position of the diverting unit, a reference transmission light pulse is coupled out of a transmission light pulse that has been guided into the monitored region.

[18] Another special advantage is that the coupling-out of the reference transmission light pulse does not limit the usable monitored region.

[19] If the diverting unit is formed by a tilted mirror, for example, which periodically guides the transmission light pulses inside a full circle in an angular range of 0° to 360° , no separate angular range need be reserved for the reference measurement. Rather, the

entire angular range covered by the transmission light pulses is available for detecting objects.

[20] A further essential advantage of the apparatus according to the invention is that the distance measurement within the entire monitored region is continuously monitored through the continuous referencing of the object detection by means of the reference measurements taken with the reference transmission light pulses.

[21] Thus, the requirements for the use of the optoelectronic apparatus in the field of security technology and personnel safety can easily be met. A notable advantage is that, with the reference measurements taken in accordance with the invention, a multi-channel design of the components for determining the transit-time differences can be omitted.

BRIEF DESCRIPTION OF THE DRAWINGS

[22] The invention is described below in conjunction with the drawings in which:

[23] Figure 1 is a longitudinal section through the optoelectronic apparatus according to the invention;

[24] Figure 2 is a cross-section through the optoelectronic apparatus according to Figure 1;

[25] Figure 3 is a longitudinal section through the exit window of the apparatus according to Figures 1 and 2, with a reflection surface for coupling out a reference transmission light pulse;

[26] Figure 4 is a first diagram for evaluating the transit times of the transmission light pulses and the reference transmission light pulses of the apparatus, according to Figures 1 through 3; and

[27] Figure 5 is a second diagram for evaluating the transit times of the transmission light pulses and the reference transmission light pulses of the apparatus according to Figures 1 through 3.

DETAILED DESCRIPTION OF THE INVENTION

[28] Figure 1 schematically illustrates the design of an embodiment of the optoelectronic apparatus 1 of the invention for detecting objects in a monitored region. Inanimate objects, as well as and especially persons entering the monitored region, are detected as objects in the monitored region.

[29] The optoelectronic apparatus 1 has a distance sensor, which operates according to the pulse-transit-time method and includes a transmitter 3 that emits transmission light pulses 2 and a receiver 5 that receives light pulses 4 reflected by an object in the monitored region. The transmitter 3 is formed by a laser diode, for example. A photodiode or the like is provided as the receiver 5.

[30] For forming the beam of the transmission light pulses 2, a transmission optics 6 is disposed downstream of the transmitter 3. For focusing the reflected light pulses 4 onto the receiver 5, a receiving optics 7 is disposed upstream of the receiver. The transmitter 3 and the receiver 5 are connected to an evaluation unit, not shown, which is formed by a microprocessor or the like.

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[31] For determining the distances of objects in the monitored region, the transit time t_0 of the received, reflected light pulses 4 that are directed at an object and reflected back to the receiver 5 are determined. In the evaluation unit, the corresponding distance values are calculated from the transit times.

[32] The transmission light pulses 2 and the received light pulses 4 reflected back from an object to the apparatus 1 are guided by a diverting unit 8. In the present embodiment, the transmission light pulses 2 are directed at the diverting unit 8 by way of a stationary mirror 9. In this embodiment, the diverting unit 8 comprises a tilted mirror 10, which is seated on a base 11 that can rotate about a vertical axis of rotation D. A motor, not shown, sets the base 11 into a rotational movement with a constant rpm. The tilted mirror 10 guides both the transmission light pulses 2 emitted by the transmitter 3 and the reception light pulses 4 reflected by an object. In principle, the diverting unit 8 can also include a plurality of tilted mirrors 10, in which instance the transmission light pulses 2 and the received, reflected light pulses 4 can be guided via separate diverting mirrors 10.

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[33] The optoelectronic apparatus 1 is integrated into a housing 12 having on its front side an exit window 13, through which the transmission light pulses 2 are guided into the monitored region, and through which the reflected light pulses 4 are guided back to the apparatus 1.

[34] As can be seen from Figure 2, the exit window 13 extends in the circumferential direction of the housing 12, along a circular arc, and over an angular range of $\Delta\alpha = 180^\circ$. The transmission light pulses 2 diverted at the diverting unit 8 are periodically guided inside the entire angular range of 360° .

[35] The transmission light pulses 2 are guided inside the angular range $\Delta\alpha$ between 0° and 180° , through the exit window 13 and into the monitored region located in a horizontal plane. A portion of the transmission light pulses 2, in contrast, are guided inside the housing 12 in the angular range between 180° and 360° .

[36] In accordance with the invention, a portion of the light quantity is coupled out of each transmission light pulse 2 as a reference transmission light pulse 2', and used for a reference measurement. To this end, the reference transmission light pulse 2' is guided, as the reference reflected light pulse 4', back to the receiver 5.

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[37] Figure 3 illustrates an example of coupling out a reference transmission light pulse 2' in this manner. In this case, a reflection surface 14 is provided in the center of the exit window 13. The width of the reflection surface 14 is significantly smaller than the beam diameter of the transmission light pulses 2. The reflection surface 14 extends in the circumferential direction over the entire length of the exit window 13. The reflection surface 14 is formed by the surface of a coating applied to the inside of the exit window 13, for example. As an alternative, a region of the exit opening 13 can be roughened to produce the reflection surface 14. In any event, the portion of a transmission light pulse 2 incident on the reflection surface 14 is reflected diffusely and guided to the receiver 5 via the diverting unit 8. Because the reflection surface 14 extends over the entire length of the exit window 13, in each angular position of the diverting unit 8, the same portion of a transmission light pulse 2 is coupled out due to reflection by the reflection surface 14, and guided as a reference reflected light pulse 4' to the receiver 5.

[38] In principle, the reference transmission light pulses 2' can also be guided from the transmitter 3 to the

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receiver 5 by way of a light waveguide or the like, not shown. The light waveguide, which is embodied, for example, as an optical fiber, has a light-entrance surface that is downstream of the transmitter 3, and by way of which a defined portion of the light quantity of a transmission light pulse 2 is coupled into the light waveguide. An advantage of this is that the reference transmission light pulse 2' need not be guided by way of the diverting unit 8, and is guided directly from the transmitter 3 to the receiver 5.

[39] In any case, the reference transmission light pulses 2' are guided completely inside the housing 12, and the reference path that is traversed by a reference transmission light pulse 2' from the transmitter 3 to the receiver 5 is known and stored as a parameter in the evaluation unit.

[40] According to the invention, for determining the distance of objects in the monitored region, the transit time t_0 of the transmitted light pulses 2 is not evaluated directly; but, the transit-time difference $t_0 - t_R$ between a transmission light pulse 2 and the respective, associated reference transmission light pulse 2' is. If the light path of the reference transmission light pulse 2' is known,

the object distance can be determined from this transit-time difference in the evaluation unit.

[41] Figures 4 and 5 illustrate two exemplary embodiments for evaluating the transit-time differences $t_o - t_R$ in respective schematic diagrams.

[42] In both cases, the analog reflected signal generated by the received, reflected light pulses 4 and reference reflected light pulses 4', respectively, that are incident on the receiver 5 are quantized. The quantized sequence E of reflection signals corresponding to the temporal course of the reception signal is then read into the individual registers R of a memory element, not shown. The memory element can be formed by a semiconductor memory or a CCD array.

[43] As shown in Figures 4 and 5, the reflection-signal sequence E containing a reflected light pulse 4 and the associated reference reflected light pulses 4' is read into the register R of the memory element. The signal values of the quantized reflection-signal sequence E stored in the individual registers R are read out cyclically by an oscillator clock and evaluated in the evaluation unit. For determining the transit-time difference $t_o - t_R$, the register positions that define the positions of the

reflected light pulse 4 or the reference reflected reception light pulse 4' are determined. If the clock rate at which the reflection-signal sequence E is read into the registers R is known, the difference between the register positions of the reflected light pulse 4 and the associated reference reflected light pulse 4' results in the transit-time difference $t_o - t_R$.

[44] Figure 4 illustrates a first embodiment of this type of evaluation. In this instance, the analog reflection signal is converted into a binary-signal sequence by a threshold-value unit, not shown. In the presence of a reflected light pulse 4 or a reference reflected light pulse 4', the reflection-signal sequence E quantized in this manner assumes the value of 1; otherwise, it assumes the value of 0. The register position that defines the position of the reflected light pulse 4 or the reference reflected light pulse 4' is preferably predetermined by the center of the respective reflected light pulse 4 or reference reflected light pulse 4'.

[45] Figure 5 depicts a second embodiment of this type of evaluation. In this case, the analog reflection signal is quantized by an analog-digital converter, also not shown. Corresponding to the word width n of the analog-

digital converter, the amplitude of the analog reflection signal is imaged onto 2^n discrete amplitude values of the quantized reflection-signal sequence E. An analog-digital converter having a word width of $n = 8$ is preferably used.

[46] Figure 5 is a schematic depiction of the amplitude courses of the reflection-signal sequence E that were generated with the analog-digital converter and appear in discrete stages, with a reflected light pulse 4 and an associated reference reflected light pulse 4'.

[47] For determining the transit-time differences $t_0 - t_R$, either the positions of the maxima or the positions of the centers of gravity of the reflected light pulse 4 and the reference reflected light pulse 4' are determined. The differences of the corresponding register positions again produce the transit-time difference $t_0 - t_R$.

[48] Because the quantizing of the analog reflection signal by means of an analog-digital converter having a sufficiently large word width yields a distinctly more detailed course of the amplitudes of the received reflected light pulses 4 and reference reflected light pulses 4' than is possible with the use of a threshold-value unit, this method of determining the transit-time difference is far more precise.

[49] As an alternative, a time-measuring module, not shown, can be used for determining the transit-time difference $t_o - t_R$. In this case, the reflected light pulse 4 and an associated reference reflected light pulse 4' are read into separate inputs of this time-measurement module. These two inputs are preferably formed by the start and stop inputs of the time-measurement module.

[50] It will be understood that the above description of the present invention is susceptible to various modifications, changes and adaptations, and the same are intended to be comprehended within the meaning and range of equivalents of the appended claims.

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